

Project Report

1. 问题: ① 油气两相、干气、黑油模型
 ② 平面、均匀、各向同性、岩石不可压、忽略毛管压力
 ③ 单井、生产井、忽略表皮效应
 ④ 边界无流动

2. 输入: ① GeoModel:

$$N_x = 11 \quad N_y = 11 \quad N_z = 1$$

$$dx = 200\text{ft} \quad dy = 100\text{ft} \quad dz = 300\text{ft}$$

$$K = 10\text{mD}, \quad \phi = 0.25, \quad \underline{D_{\text{top}} = 5000\text{ft}}$$

- ② Well:

$$(6, 6, 1)$$

$$\begin{cases} \text{BHP} > 2000\text{psi} & , \quad \text{OilRate} = 5000 \text{ BBLs/day} \\ \text{BHP} \leq 2000\text{psi} & , \quad \text{BHP} = 2000\text{psi} \end{cases}$$

$$T = 1000\text{days}$$

$$\text{radius} = 0.25\text{ft}$$

- ③ PVT:

$$C_R = 0$$

$$P_{\text{oil}} = 46.244 \text{ lbm/scf}, \quad P_{\text{water}} = 62.238 \text{ lbm/scf}, \quad P_{\text{gas}} = 0.0647 \text{ lbm/s}$$

$$\mu_o = 6e-8 p^2 - 4.589e-4 p + 1.1179 \quad (\text{psi}; \text{cp})$$

$$\mu_g = 3e-10 p^2 + 1e-6 p + 0.0133 \quad (\text{psi}; \text{cp})$$

$$B_o = -3.922264e-8 p^2 + 0.0003 p + 1 \quad (\text{psi}; 1)$$

$$B_g = 3592.7 p \wedge (-1.0226) \quad (\text{psi}; 1)$$

$$k_{ro} = \begin{cases} 0 & , \quad S_g \geq 0.85 \\ \left(\frac{0.85 - S_g}{0.85} \right)^{1.5} & , \quad S_g \leq 0.85 \end{cases}$$

$$k_{rg} = \begin{cases} 0.85 \wedge 1.5 & , \quad S_g \geq 0.85 \\ S_g \wedge 1.5 & , \quad S_g \leq 0.85 \end{cases}$$

$$R_s = \begin{cases} 1 & , \quad P > 3824.321712 \\ 0.0000476 P \wedge 1.206511 & , \quad P < 2074.271712 \end{cases} \quad (\text{psi}; \frac{\text{mscf}}{\text{cTR}})$$

④ Initial Condition:

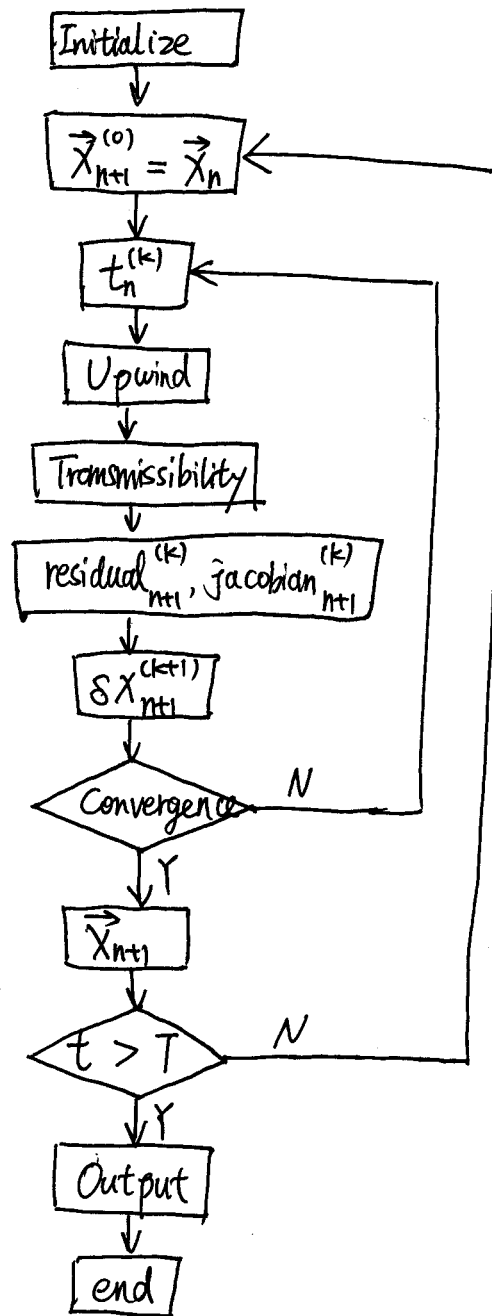
$$p = 5039.623 \text{ psi}$$

$$S_g = 0$$

⑤ Boundary Condition:

No flow

3. 流程图



4. 离散方程

1. 组分质量守恒方程

$$\sum_l m_{\bar{o},0} \bullet m_{\bar{o},0}^w = \frac{1}{\Delta t} \Delta_t M_{\bar{o},0}$$

$$\left(\sum_l m_{\bar{g},g} + \sum_l m_{\bar{g},0} \right) - (m_{\bar{g},g}^w + m_{\bar{g},0}^w) = \frac{1}{\Delta t} \Delta_t (M_{\bar{g},g} + M_{\bar{g},0})$$

2. 离散方程

$$\begin{aligned} & \left(\frac{\lambda_o}{B_o} T_o \right)_{t-\frac{1}{2}} (P_{o,i-1} - P_{o,i}) \\ & + \left(\frac{\lambda_o}{B_o} T_o \right)_{t+\frac{1}{2}} (P_{o,i+1} - P_{o,i}) \\ & + \left(\frac{\lambda_o}{B_o} T_o \right)_{j-\frac{1}{2}} (P_{o,j-1} - P_{o,j}) \\ & + \left(\frac{\lambda_o}{B_o} T_o \right)_{j+\frac{1}{2}} (P_{o,j+1} - P_{o,j}) \\ & - (q_o^w)_i = \frac{dV \cdot \phi}{C_{UnitConversion} \cdot dt} \left[\left(\frac{S_o}{B_o} \right)^{n+1} - \left(\frac{S_o}{B_o} \right)^n \right] \\ & \left(\frac{\lambda_g}{B_g} T_g + \frac{\lambda_o}{B_o} T_o \cdot R_s \right)_{t-\frac{1}{2},j} (P_{g,t+1,j} - P_{g,t,j}) \\ & + \left(\frac{\lambda_g}{B_g} T_g + \frac{\lambda_o}{B_o} T_o \cdot R_s \right)_{t+\frac{1}{2},j} (P_{g,t+1,j} - P_{g,t,j}) - (q_g^w + R_s \cdot q_o^w) \\ & + \left(\frac{\lambda_g}{B_g} T_g + \frac{\lambda_o}{B_o} T_o \cdot R_s \right)_{i,j-\frac{1}{2}} (P_{g,t,j-1} - P_{g,t,j}) \\ & + \left(\frac{\lambda_g}{B_g} T_g + \frac{\lambda_o}{B_o} T_o \cdot R_s \right)_{i,j+\frac{1}{2}} (P_{g,t,j+1} - P_{g,t,j}) \\ & = \frac{dV \cdot \phi}{C_{UnitConversion} \cdot dt} \left[\left(\frac{S_g}{B_g} + R_s \frac{S_o}{B_o} \right)^{n+1} - \left(\frac{S_g}{B_g} + R_s \frac{S_o}{B_o} \right)^n \right] \end{aligned}$$

传导率: $\gamma_o(p, S_g) \equiv \frac{\lambda_o}{B_o} T_o$, $\gamma_g \equiv \frac{\lambda_g}{B_g} T_g$

$\gamma = \text{GeoTerm} * \text{FluidTerm}$

比如, $\text{GeoTerm } X = \frac{k \cdot dy \cdot dz}{dx}$

$(\text{FluidTerm Oil})_{t+\frac{1}{2},j} = \begin{cases} \left(\frac{k_{ro}}{B_o \mu_o} \right)_{ij}, & P_{o,ij} > P_{o,t+1,j} \\ \left(\frac{k_{ro}}{B_o \mu_o} \right)_{t+1,ij}, & P_{o,ij} < P_{o,t+1,j} \end{cases}$

#传导: 定义 γ_o^w 为 $q_o^w = \gamma_o^w (p_o - p^w)$, 则

$$\gamma_o^w(p, s, q) = WI \cdot \lambda_o$$

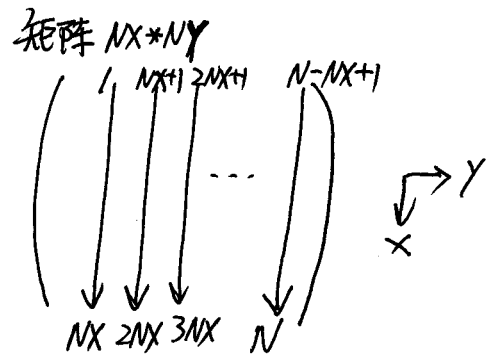
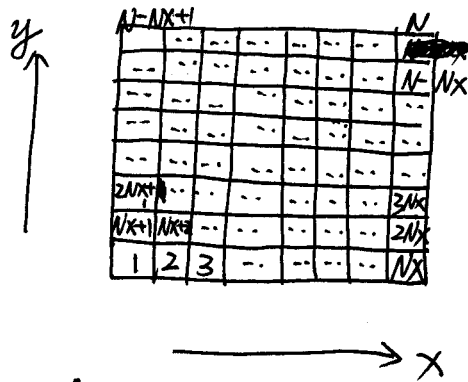
其中 $WI = \frac{2\pi k dz}{\ln(\frac{r_o}{r_w})}$

$$r_o = 0.14 \sqrt{dx^2 + dy^2}$$

$$\lambda_o = \frac{k r_o}{\mu_o \cdot B_o}$$

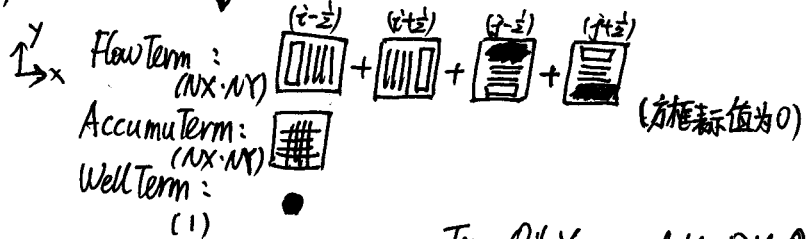
3. 计算模型

① 坐标图:



② Residual vector

Residual $(2N \times 1)$ = Residual Oil $(NX \cdot NY)$; Residual Gas $(NX \cdot NY)$



比如, $FlowTermOil_XPlus = TransOilX \cdot \Delta PX$

$TransOilX = GeoTermX \cdot FluidTermOilX$

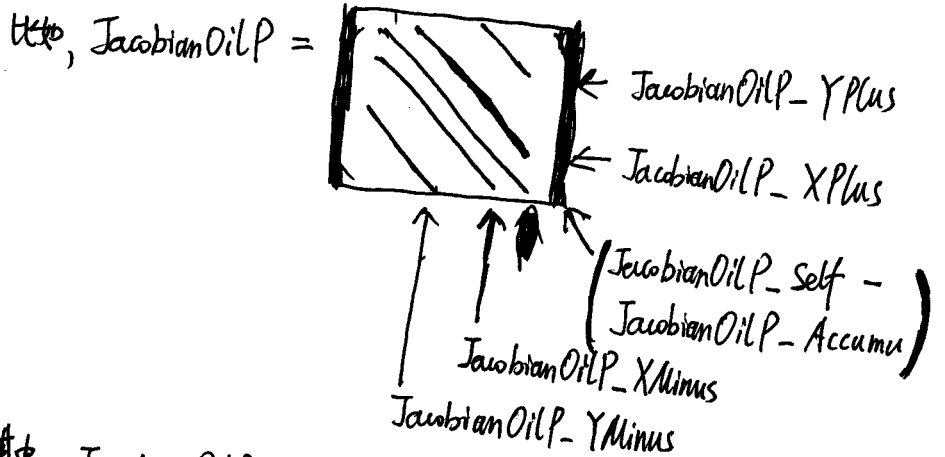
$\Delta PX = FluidTermOilX - FluidTermOil(upwindXPlus)$

$FlowTermOil_XMinus = TransOilX \cdot (-\Delta PX)$ (矩阵沿图上面的值)

$$\text{Accumu Term Oil} = \frac{dV \cdot \phi}{C \cdot dt} \cdot (S_0 \cdot B_0 - S_{0-Previous} \cdot B_{0-Pre})$$

③ Jacobian

$$\text{Jacobian} = \begin{matrix} \text{Jacobian Oil P} & \text{Jacobian Oil Seg} \\ \text{---} & \text{---} \\ (2N \times 2N) & \text{Jacobian Gas P} & \text{Jacobian Gas Seg} \end{matrix}$$



其中, Jacobian Oil P - Self =

~~其中~~ $x^+ = \text{upwind X Plus - Self} \cdot \left(\frac{\partial \text{Trans Oil X}}{\partial P} \right) \cdot \text{delta PX}$





- Trans Oil X

Jacobian Oil P - X Plus = $\text{upwind X Plus - Other} \cdot \left(\frac{\partial \text{Trans Oil X}}{\partial P} \right) \cdot \text{delta PX}$

+ Trans Oil X


~~xxxxxx~~

$$\textcircled{x} = \text{upwindXPlus_Other} \cdot \left(\frac{\partial \text{TransOilX}}{\partial p} \right) \cdot (-\text{deltaPX})$$

(取矩阵中值)

- TransOilX



$$\text{JacobianOilP_XMinus} = \text{upwindXPlus_Self} \cdot \left(\frac{\partial \text{TransOilX}}{\partial p} \right) \cdot (-\text{deltaPX})$$



+ TransOilX



(矩阵全部沿用前面的值)

$$\text{JacobianOilP_Accumu} = \frac{dW \cdot \phi}{C \cdot dt} \cdot \left(-s_0 \cdot \text{difBo} / \text{Bo}^2 \right)$$



其中 upwindXPlus_Self, upwindXPlus_Other 是迎风状态因子。



$(NX-1) * NY$

- Note:
1. 气方程井项 PVT 参数使用 PBlock 计算 (或者应该是把井也视为一个网络),
用迎风格式计算。
Rs
 2. ECLIPSE 计算效率明显优于我的程序。

- Problems:
1. 块五对角矩阵快速解法 / 高精度解法。
 2. 大条件数方程如何可能得到高精度解?

