

第8章 平面问题的极坐标解法

8.1 力学方程组

1° 几何方程

$$\begin{aligned} \nabla \vec{u} &= \left(\vec{e}_r \frac{\partial}{\partial r} + \frac{\vec{e}_\theta}{r} \frac{\partial}{\partial \theta} \right) (u_r \vec{e}_r + u_\theta \vec{e}_\theta) \\ &= \vec{e}_r \vec{e}_r \frac{\partial u_r}{\partial r} + \vec{e}_r \vec{e}_\theta \frac{\partial u_\theta}{\partial r} + \frac{1}{r} \vec{e}_\theta \left(\frac{\partial u_r}{\partial \theta} \vec{e}_r + u_r \vec{e}_\theta \right) \\ &\quad + \frac{1}{r} \vec{e}_\theta \left(\frac{\partial u_\theta}{\partial \theta} \vec{e}_\theta + u_\theta (-\vec{e}_r) \right) \\ &= \vec{e}_r \vec{e}_r \frac{\partial u_r}{\partial r} + \vec{e}_r \vec{e}_\theta \frac{\partial u_\theta}{\partial r} + \vec{e}_\theta \vec{e}_r \left(\frac{1}{r} \frac{\partial u_r}{\partial \theta} - \frac{1}{r} u_\theta \right) \\ &\quad + \vec{e}_\theta \vec{e}_\theta \left(\frac{1}{r} u_r + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} \right) \end{aligned}$$

代入张量形式的几何方程 $\vec{\Gamma} = \frac{1}{2}(\nabla \vec{u} + \vec{u} \nabla)$ 得

$$\begin{cases} \epsilon_r = \frac{\partial u_r}{\partial r} \\ \epsilon_\theta = \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{u_r}{r} \\ \epsilon_{r\theta} = \frac{1}{2} \left(\frac{\partial u_\theta}{\partial r} + \frac{1}{r} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta}{r} \right) \end{cases}$$

附加项
(由坐标基函数非零引起)

2° 平衡方程

$$\begin{aligned} \nabla \cdot \vec{T} &= \left(\vec{e}_r \frac{\partial}{\partial r} + \frac{1}{r} \vec{e}_\theta \frac{\partial}{\partial \theta} \right) \cdot (\sigma_r \vec{e}_r \vec{e}_r + \sigma_\theta \vec{e}_\theta \vec{e}_\theta + \tau_{r\theta} \vec{e}_r \vec{e}_\theta + \tau_{\theta r} \vec{e}_\theta \vec{e}_r) \\ &= \frac{\partial \sigma_r}{\partial r} \vec{e}_r + \frac{\partial \tau_{r\theta}}{\partial r} \vec{e}_\theta + \frac{1}{r} \vec{e}_\theta \cdot (\sigma_r \vec{e}_\theta \vec{e}_r + \frac{\partial \sigma_\theta}{\partial \theta} \vec{e}_\theta \vec{e}_\theta + \sigma_\theta \vec{e}_\theta (-\vec{e}_r) + \tau_{r\theta} \vec{e}_\theta \vec{e}_\theta + \frac{\partial \tau_{\theta r}}{\partial \theta} \vec{e}_\theta \vec{e}_r + \tau_{\theta r} \vec{e}_\theta \vec{e}_\theta) \\ &= \vec{e}_r \left(\frac{\partial \sigma_r}{\partial r} + \frac{\sigma_r}{r} - \frac{\sigma_\theta}{r} + \frac{1}{r} \frac{\partial \tau_{\theta r}}{\partial \theta} \right) + \vec{e}_\theta \left(\frac{\partial \tau_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_\theta}{\partial \theta} + \frac{2\tau_{r\theta}}{r} \right) \end{aligned}$$

代入平衡方程 $\nabla \cdot \vec{T} + \vec{f} = 0$ 得

$$\begin{cases} \frac{\partial \sigma_r}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\theta}}{\partial \theta} + \frac{\sigma_r - \sigma_\theta}{r} + f_r = 0 \\ \frac{\partial \tau_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_\theta}{\partial \theta} + \frac{2\tau_{r\theta}}{r} + f_\theta = 0 \end{cases}$$

附加项
(由坐标基函数非零引起)

3° 本构关系

因为弹性体是各向同性的，极坐标下的本构关系与直角坐标下的本构关系有相同的形式。

应力表示的本构关系：

$$\begin{cases} \epsilon_r = \frac{1}{E} (\sigma_r - \nu \sigma_\theta) \\ \epsilon_\theta = \frac{1}{E} (\sigma_\theta - \nu \sigma_r) \\ \epsilon_{r\theta} = \frac{1+\nu}{E} \tau_{r\theta} \end{cases}$$

应变表示的本构关系：

$$\begin{cases} \sigma_r = \frac{E}{1-\nu^2} (\epsilon_r + \nu \epsilon_\theta) \\ \sigma_\theta = \frac{E}{1-\nu^2} (\epsilon_\theta + \nu \epsilon_r) \\ \tau_{r\theta} = \frac{E}{1+\nu} \epsilon_{r\theta} \end{cases}$$

对平面应变问题，需作代换 $E' = \frac{E}{1-\nu^2}$, $\nu' = \frac{\nu}{1-\nu}$

4° Airy 应力函数

由“应力函数”一节知，Airy 应力函数与应力张量间满足关系：

$$\vec{T} = \nabla \times \vec{k} \vec{k} (-U) \times \nabla$$

对平面问题， $\nabla = \vec{e}_r \frac{\partial}{\partial r} + \frac{1}{r} \vec{e}_\theta \frac{\partial}{\partial \theta}$ ，得

$$\begin{aligned} \vec{T} &= \left\{ \left(\vec{e}_r \frac{\partial}{\partial r} + \frac{1}{r} \vec{e}_\theta \frac{\partial}{\partial \theta} \right) \times \left[\vec{e}_r \vec{e}_r (-U) \right] \right\} \times \left(\vec{e}_r \frac{\partial}{\partial r} + \frac{1}{r} \vec{e}_\theta \frac{\partial}{\partial \theta} \right) \\ &= \vec{e}_r \vec{e}_r \left(\frac{1}{r} \frac{\partial U}{\partial r} + \frac{1}{r^2} \frac{\partial^2 U}{\partial \theta^2} \right) + \vec{e}_\theta \vec{e}_\theta \frac{\partial^2 U}{\partial r^2} \\ &\quad + \vec{e}_r \vec{e}_\theta \left[-\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial U}{\partial \theta} \right) \right] + \vec{e}_\theta \vec{e}_r \left[-\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial U}{\partial \theta} \right) \right] \end{aligned}$$

得到应力分量与应力函数间关系

$$\begin{cases} \sigma_r = \frac{1}{r} \frac{\partial U}{\partial r} + \frac{1}{r^2} \frac{\partial^2 U}{\partial \theta^2} \\ \sigma_\theta = \frac{\partial^2 U}{\partial r^2} \quad \leftarrow \text{附加项} \\ \tau_{r\theta} = -\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial U}{\partial \theta} \right) \end{cases}$$

将应力分量代入应力协调方程(见6°)，可得应力函数 U 满足 $\nabla^2 \nabla^2 U = 0$
原弹性力学问题转化为了双调和方程的边值问题。

5° 应变协调方程 $(\nabla \times (\nabla \times \nabla) = -\vec{k} \vec{k} L_{33}) = 0$

$$\left(\frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} - \frac{1}{r} \frac{\partial}{\partial r}\right) \varepsilon_r + \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \varepsilon_\theta}{\partial r}\right) - \frac{2}{r^2} \frac{\partial}{\partial r} \left(r \frac{\partial \varepsilon_{r\theta}}{\partial \theta}\right) = 0$$

6° 应力协调方程.

无体力或体力为常值时, 平面问题应力协调方程的直角坐标形式为

$$\nabla^2 (\sigma_x + \sigma_y) = 0$$

对平面问题, $\tau_{zx} = \tau_{zy} = 0$, 此时 $\sigma_x + \sigma_y$ 是不变量.

所以, 对于极坐标, 应力协调方程为

$$\nabla^2 (\sigma_r + \sigma_\theta) = 0$$

$$\text{其中 } \nabla^2 = \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2}$$

8.2 轴对称应力

如果各应力呈轴对称分布, 也就是与 θ 无关, 则应力函数 $U = U(r)$.

$$\text{双调和方程变为 } \left(\frac{d^2}{dr^2} + \frac{1}{r} \frac{d}{dr}\right)^2 U = 0$$

$$\text{化简得 } r^4 U^{(4)} + 2r^3 U^{(3)} - r^2 U^{(2)} + r U^{(1)} = 0$$

这是一个四阶 Euler 方程.

$$\text{引入变换 } r = e^t, \text{ 得 } \frac{d^4 U}{dt^4} - 4 \frac{d^3 U}{dt^3} + 4 \frac{d^2 U}{dt^2} = 0$$

$$\text{通解为 } U = At + Bte^{2t} + Ce^{2t} + D$$

作反变换 $t = \ln r$, 得通解

$$U = A \ln r + Br^2 \ln r + Cr^2 + D$$

由应力与应力函数的关系可得应力场

$$\begin{cases} \sigma_r = \frac{1}{r} \frac{dU}{dr} = \frac{A}{r^2} + B(1 + 2 \ln r) + 2C \\ \sigma_\theta = \frac{d^2 U}{dr^2} = -\frac{A}{r^2} + B(3 + 2 \ln r) + 2C \\ \tau_{r\theta} = 0 \end{cases}$$

位移场: 由几何方程和本构关系可得

$$\frac{\partial u_r}{\partial r} = \frac{1}{E} \left[(1+\nu) \frac{A}{r^2} + (1-3\nu)B + 2(1-\nu)B \ln r + 2(1-\nu)C \right]$$

$$\bullet \frac{u_r}{r} + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} = \frac{1}{E} \left[-(1+\nu) \frac{A}{r^2} + (3-\nu)B + 2(1-\nu)B \ln r + 2(1-\nu)C \right]$$

$$\frac{1}{r} \frac{\partial u_r}{\partial \theta} + \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r} = 0$$

积分第1式, 得

$$u_r = \frac{1}{E} \left[-(1+\nu) \frac{A}{r} + (1-3\nu)Br + 2(1-\nu)B r (\ln r - 1) + 2(1-\nu)Cr \right] + f(\theta)$$

代入第2式, 得

$$\frac{\partial u_\theta}{\partial \theta} = \frac{4Br}{E} - f(\theta)$$

积分得

$$u_\theta = \frac{4Br\theta}{E} - \int f(\theta) d\theta + g(r)$$

将上述 u_r, u_θ 代入第3式, 得

$$\frac{1}{r} \frac{df(\theta)}{d\theta} + \frac{dg(r)}{dr} - \frac{g(r)}{r} + \frac{1}{r} \int f(\theta) d\theta = 0$$

或者 $g(r) - r \frac{dg(r)}{dr} = \frac{df(\theta)}{d\theta} + \int f(\theta) d\theta$

所以
$$\begin{cases} g(r) - r \frac{dg(r)}{dr} = F \\ \frac{df(\theta)}{d\theta} + \int f(\theta) d\theta = F \end{cases} \quad (F \text{ 是常数})$$

得到通解
$$\begin{cases} g(r) = Hr + F \\ f(\theta) = I \sin \theta + k \cos \theta \end{cases}$$

位移场为

$$\begin{cases} u_r = \frac{1}{E} \left[-(1+\nu) \frac{A}{r} + (1-3\nu)Br + 2(1-\nu)Br (\ln r - 1) + 2(1-\nu)Cr \right] + I \sin \theta + k \cos \theta \\ u_\theta = \frac{4Br\theta}{E} + Hr + I \cos \theta - k \sin \theta \end{cases}$$

注：上述位移场表示，应力轴对称，不一定有位移轴对称。

2° 如果应力轴对称、物体几何形状轴对称、(应力(或几何约束)轴对称)，^轴则位移轴对称。

在不考虑刚体位移下，上述系数满足 $B=H=I=K=0$ 。

$$\text{应力场: } \begin{cases} \sigma_r = \frac{A}{r^2} + 2C \\ \sigma_\theta = -\frac{A}{r^2} + 2C \\ \tau_{r\theta} = 0 \end{cases}$$

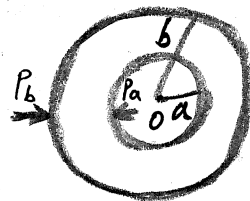
$$\text{位移场: } \begin{cases} u_r = \frac{1}{E} [-(1+\nu)\frac{A}{r} + 2(1-\nu)Cr] \\ u_\theta = 0 \end{cases}$$

3° 上述位移场是针对平面应力问题的。对于平面应变问题，需作代换

$$E' = \frac{E}{1-\nu^2}, \quad \nu' = \frac{\nu}{1-\nu}$$

8-3 厚壁圆筒受均匀分布压力作用

厚壁圆筒内外半径分别为 a, b ，筒受内压 P_a ，外压 P_b 。



这是一个无体力的平面应变问题，

原弹性力学边值问题变成应力函数的边值问题：

$$\begin{cases} \nabla^2 \nabla^2 U = 0 & (a \leq r \leq b) \\ \sigma_r(a, \theta) = -P_a, \quad \tau_{r\theta}(a, \theta) = 0 \\ \sigma_r(b, \theta) = -P_b, \quad \tau_{r\theta}(b, \theta) = 0 \end{cases}$$

这是一个应力轴对称问题，解法同 8-2。

应用 8-2 注 2° 的结果，待定系数满足

$$\begin{cases} \frac{A}{a^2} + 2C = -P_a \\ \frac{A}{b^2} + 2C = -P_b \end{cases} \quad \text{解得} \quad \begin{cases} A = \frac{a^2 b^2}{b^2 - a^2} (P_b - P_a) \\ C = \frac{a^2 P_a - b^2 P_b}{2(b^2 - a^2)} \end{cases}$$

$$\text{得应力场} \quad \begin{cases} \sigma_r = \frac{a^2}{b^2 - a^2} \left(1 - \frac{b^2}{r^2}\right) P_a - \frac{b^2}{b^2 - a^2} \left(1 - \frac{a^2}{r^2}\right) P_b \\ \sigma_\theta = \frac{a^2}{b^2 - a^2} \left(1 + \frac{b^2}{r^2}\right) P_a - \frac{b^2}{b^2 - a^2} \left(1 + \frac{a^2}{r^2}\right) P_b \\ \tau_{r\theta} = 0 \end{cases}$$

注: 1° 对有圆孔的无限大板在无界远处受双向拉伸的情况,

可令 $b \rightarrow \infty$, $P_a = 0$, 且记 $P_\infty = -P_b$.

$$\text{则应力场为 } \begin{cases} \sigma_r = (1 - \frac{a^2}{r^2}) P_\infty \\ \sigma_\theta = (1 + \frac{a^2}{r^2}) P_\infty \\ \tau_{r\theta} = 0 \end{cases}$$

定义应力集中系数 $k = \frac{(\sigma_\theta)_{\max}}{P_\infty}$,

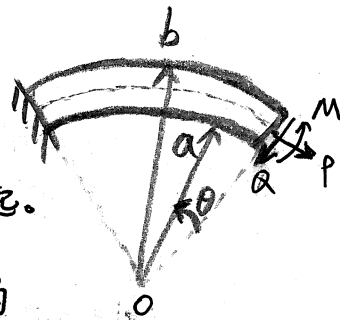
则 $k = 2$, 在 $r = a$ 达到.

8.4 曲梁

矩形截面曲梁内外半径分别为 a, b .

端部受轴力 P , 剪力 Q , 弯矩 M .

曲率中心 O 为坐标原点, 极角从右端量起.



这是一个无体力的平面应力问题, 转化为

应力函数的边值问题:

$$\begin{cases} \nabla^2 \nabla^2 U = 0 \\ \sigma_r(a, \theta) = 0, \tau_{r\theta}(a, \theta) = 0 \\ \sigma_r(b, \theta) = 0, \tau_{r\theta}(b, \theta) = 0 \\ \int_a^b \sigma_\theta(r, 0) dr = P, \\ \int_a^b \tau_{r\theta}(r, 0) dr = Q, \\ \int_a^b \sigma_\theta(r - \frac{a+b}{2}) dr = -M \end{cases}$$

应力函数: 应力函数可以表示为 P, Q, M 的线性函数

$$U(r, \theta) = P U_1(r, \theta) + Q U_2(r, \theta) + M U_3(r, \theta)$$

$$\text{其中 } \begin{cases} U_1 = f(r) \cos \theta - \frac{a+b}{2} g(r) \\ U_2 = -f(r) \sin \theta \\ U_3 = g(r) \end{cases}$$

推导见 [王] P259.

注: 1° 理解解法: M : 应力轴对称

$$\begin{cases} Q: M(\theta) = -Q \sin \theta \quad (\text{回想应力函数的性质3}) \\ P: U_1(r, \theta + \frac{\pi}{2}) = U_2(r, \theta) - \frac{a+b}{2} U_3(r, \theta) \end{cases}$$

① 纯弯曲

这是一个轴对称应力问题。

$$\text{应力场} \begin{cases} \sigma_r = \frac{A}{r^2} + B(1+2\ln r) + 2C \\ \sigma_\theta = -\frac{A}{r^2} + B(3+2\ln r) + 2C \\ \tau_{r\theta} = 0 \end{cases}$$

代入边界条件得

$$\begin{cases} \frac{A}{a^2} + 2B\ln a + B + 2C = 0 \\ \frac{A}{b^2} + 2B\ln b + B + 2C = 0 \\ b\left(\frac{A}{b^2} + 2B\ln b + B + 2C\right) - a\left(\frac{A}{a^2} + 2B\ln a + B + 2C\right) = 0 \\ A\ln\frac{b}{a} - B(b^2 - a^2) - B(b^2\ln b - a^2\ln a) - C(b^2 - a^2) = M \end{cases}$$

$$\text{解得} \begin{cases} A = -\frac{4M}{N} a^2 b^2 \ln\frac{b}{a} \\ B = -\frac{2M}{N} (b^2 - a^2) \\ C = \frac{M}{N} [b^2 - a^2 + 2(b^2\ln b - a^2\ln a)] \end{cases}$$

$$\text{其中 } N = (b^2 - a^2)^2 - 4a^2 b^2 \left(\ln\frac{b}{a}\right)^2$$

应力场为

$$\begin{cases} \sigma_r = -\frac{4M}{N} \left(\frac{a^2 b^2}{r^2} \ln\frac{b}{a} + b^2 \ln\frac{r}{b} - a^2 \ln\frac{r}{a} \right) \\ \sigma_\theta = -\frac{4M}{N} \left(-\frac{a^2 b^2}{r^2} \ln\frac{b}{a} + b^2 \ln\frac{r}{b} - a^2 \ln\frac{r}{a} + b^2 - a^2 \right) \\ \tau_{r\theta} = 0 \end{cases}$$

注：① 位移场也可套用 8-2 节结论得出，形式较繁且没必要，故略去。

位移场中的常数 H, I, K 由梁的约束条件确定。

② 有小角度缺口的圆环初应力问题：

不连续环具有小切口，切口圆心角为 α ，焊接成整环。

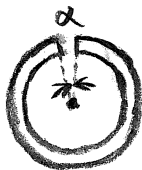
环向位移 $u_\theta = \alpha r$

由梁纯弯曲问题的位移场知， $\theta = 2\pi$ 的端面环向位移

$$u_\theta = \frac{8Br\pi}{E}, \text{ 得 } B = \frac{\alpha E}{8\pi}$$

由 $B = -\frac{2M}{N}(b^2 - a^2)$ 得

$$\text{预应力为力矩 } M = -\frac{\alpha E}{8\pi} \frac{(b^2 - a^2)^2 - 4a^2 b^2 \left(\ln\frac{b}{a}\right)^2}{2(b^2 - a^2)}$$



楔形位移

② 切向力

设应力函数 $U = f(r) \sin \theta$

应力场: 由双调和方程 $\nabla^2 \nabla^2 U = 0$ 得

$$\left(\frac{d^2}{dr^2} + \frac{1}{r} \frac{d}{dr} - \frac{1}{r^2} \right)^2 U = 0$$

展开得

$$f'''' + \frac{2}{r} f''' - \frac{3}{r^2} f'' + \frac{3}{r^3} f' - \frac{3}{r^4} f = 0$$

引入变换 $r = e^t$ 得

$$f^{(4)} - 4f^{(3)} + 2f^{(2)} + 4f^{(1)} - 3f = 0$$

解得 $f(t) = e^t, te^t, e^{-t}, e^{3t}$

作反变换 $t = \ln r$ 得

$$f(r) = r, r \ln r, \frac{1}{r}, r^3$$

通解为

$$f(r) = Ar + \frac{B}{r} + Cr^3 + Dr \ln r$$

由应力与应力函数间关系, 得应力场

$$\left\{ \begin{aligned} \sigma_r &= \frac{1}{r} \frac{\partial U}{\partial r} + \frac{1}{r^2} \frac{\partial^2 U}{\partial \theta^2} \\ &= \left(-\frac{2B}{r^3} + 2Cr + \frac{D}{r} \right) \sin \theta \\ \sigma_\theta &= \frac{\partial^2 U}{\partial r^2} \\ &= \left(\frac{2B}{r^3} + 6Cr + \frac{D}{r} \right) \sin \theta \\ \tau_{r\theta} &= -\frac{\partial}{\partial r} \left(\frac{\partial U}{\partial \theta} \right) \\ &= \left(\frac{2B}{r^3} - 2Cr - \frac{D}{r} \right) \cos \theta \end{aligned} \right.$$

代入应力边界条件, 得

~~2B + 2a^4 C + a^2 D = 0~~

$$\left\{ \begin{aligned} -2B + 2a^4 C + a^2 D &= 0 \\ -2B + 2b^4 C + b^2 D &= 0 \\ \left(\frac{1}{b^2} - \frac{1}{a^2} \right) B + (b^2 - a^2) \frac{C}{4} \left(\ln \frac{b}{a} \right) D &= -Q \end{aligned} \right.$$

解得 $\begin{cases} B = -\frac{Q}{2k} a^2 b^2 \\ C = \frac{Q}{2k} \\ D = -\frac{a^2 + b^2}{4} Q \end{cases}$ 其中 $k = a^2 - b^2 + (a^2 + b^2) \ln \frac{b}{a}$

先求 $\nabla^2 U$,
再求 $\nabla^2(\nabla^2 U)$,
这样不容易出错

得应力场:

$$\begin{cases} \sigma_r = \frac{Q}{K} \left(\frac{a^2 b^2}{r^3} + r - \frac{a^2 + b^2}{r} \right) \sin \theta \\ \sigma_\theta = \frac{Q}{K} \left(-\frac{a^2 b^2}{r^3} + 3r - \frac{a^2 + b^2}{r} \right) \sin \theta \\ \tau_{r\theta} = \frac{Q}{K} \left(-\frac{a^2 b^2}{r^3} - r + \frac{a^2 + b^2}{r} \right) \cos \theta \end{cases}$$

位移场:

由平面应力问题的本构方程和几何方程, 得

$$\begin{cases} \frac{\partial u_r}{\partial r} = \frac{\sin \theta}{E} \left[-(1+\nu) \frac{2B}{r^3} + (1-3\nu) 2Cr + (1-\nu) \frac{D}{r} \right] \\ \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{u_r}{r} = \frac{\sin \theta}{E} \left[(1+\nu) \frac{2B}{r^3} + (3-\nu) 2Cr + (1-\nu) \frac{D}{r} \right] \\ \frac{\partial u_\theta}{\partial r} + \frac{1}{r} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta}{r} = \frac{2(1+\nu)}{E} \cos \theta \left(\frac{2B}{r^3} - 2Cr - \frac{D}{r} \right) \end{cases}$$

积为第一式, 得

$$u_r = \frac{\sin \theta}{E} \left[(1+\nu) \frac{B}{r^2} + (1-3\nu) Cr^2 + (1-\nu) D \ln r \right] + f(\theta)$$

代入第二式, 并积为得

$$u_\theta = -\frac{\cos \theta}{E} \left[(1+\nu) \frac{B}{r^2} + (5+\nu) Cr^2 + (1-\nu) D (1 - \ln r) \right] - \int f(\theta) d\theta + g(r)$$

将 u_r, u_θ 代入第三式得

$$f'(\theta) + \int f(\theta) d\theta + \frac{4D}{E} \cos \theta = g(r) - r g'(r)$$

所以

$$\begin{cases} f'(\theta) + \int f(\theta) d\theta + \frac{4D}{E} \cos \theta = F \\ g(r) - r g'(r) = F \end{cases}$$

通解为

$$\begin{cases} f(\theta) = -\frac{2D}{E} \theta \cos \theta + K \sin \theta + L \cos \theta \\ g(r) = Hr + F \end{cases}$$

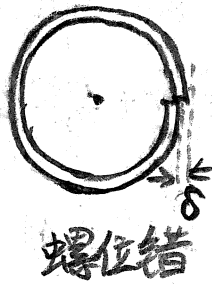
得位移场

$$u_r = -\frac{2D}{E} \theta \cos \theta + \frac{\sin \theta}{E} \left[(1+\nu) \frac{B}{r^2} + (1-3\nu) Cr^2 + (1-\nu) D \ln r \right] + K \sin \theta + L \cos \theta$$

$$u_\theta = \frac{2D}{E} \theta \sin \theta - \frac{\cos \theta}{E} \left[(1+\nu) \frac{B}{r^2} + (5+\nu) Cr^2 - (1+\nu) D - (1-\nu) D \ln r \right] + K \cos \theta - L \sin \theta + Hr$$

其中 K, L, H 对应刚体位移 (平移, 转动)

注: 1. 有径向错位的圆环初应力问题.



圆环沿径向切开, 错开 δ 长度后焊接起来.

径向错位 $u_r|_0^{2\pi} = \delta$

由切向力下曲梁的位移场知

$$u_r|_0^{2\pi} = -\frac{4\pi D}{E}$$

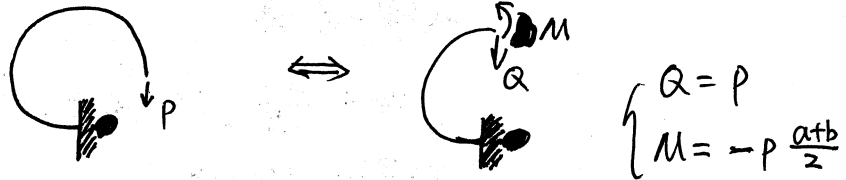
$$\therefore D = -\frac{\delta E}{4\pi}$$

由 $D = -\frac{a^2 b^2}{k} Q$ 得

预应力为切向力

$$Q = E \frac{a^2 - b^2 + (a^2 + b^2) \ln \frac{b}{a}}{4\pi (a^2 + b^2)} \delta$$

③ 法向力



如图所示, 曲梁受法向力的问题可以转化为纯弯曲和切向力问题的叠加。Q, M 的取值已给出。

记纯弯曲问题中的待定系数有下标 "1", 切向力问题中的待定系数有下标 "2"。

原问题的结果可由 "1", "2" 的结果相加, 并作代换 $\theta \rightarrow \theta + \frac{\pi}{2}$ 得出。

应力场:

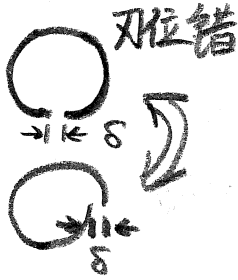
$$\sigma_r = \left[\frac{A_1}{r^2} + B_1(1 + 2 \ln r) + 2C_1 \right] + \left[-\frac{2B_2}{r^3} + 2C_2 r + \frac{D_2}{r} \right] \cos \theta$$

$$\sigma_\theta = \left[-\frac{A_1}{r^2} + B_1(3 + 2 \ln r) + 2C_1 \right] + \left[\frac{2B_2}{r^3} + 6C_2 r + \frac{D_2}{r} \right] \cos \theta$$

$$\tau_{r\theta} = -\left[\frac{2B_2}{r^3} - 2C_2 r - \frac{D_2}{r} \right] \sin \theta$$

位移场略去。

注: 1° 有平行切口的圆环初应力问题



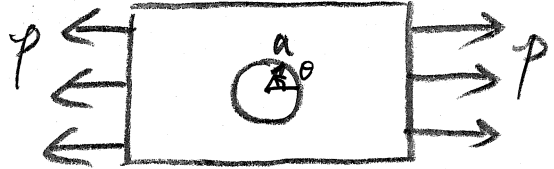
不完整圆环有小缺口, 切口平行, 距离为 δ , 焊接成整环。
问题可以化为螺~~纹~~位错问题。

如图, 原问题可以化为在另一个位置产生径向错位 δ (向外) 的预应力问题。预应力只在此前已给出。

欲求整个环上的预应力分布, 可由平衡关系得出。

8.5 具有圆孔的无限大平板之拉伸

一个相当大的薄板, 中心有一个半径为 a 的小孔, 在无穷远处有沿 x 方向的均匀拉力 p 。



直角坐标系下的应力边界条件为

$$\begin{cases} \sigma_x(\pm\infty, y) = p \\ \sigma_y(\pm\infty, y) = 0 \\ \tau_{xy}(\pm\infty, y) = 0 \end{cases}$$

由应力分量对应关系

$$\begin{cases} \sigma_r = (\cos\theta, \sin\theta) \begin{pmatrix} \sigma_x & \tau_{xy} \\ \tau_{xy} & \sigma_y \end{pmatrix} \begin{pmatrix} \cos\theta \\ \sin\theta \end{pmatrix} = \sigma_x \cos^2\theta + \sigma_y \sin^2\theta + 2\tau_{xy} \sin\theta \cos\theta \\ \sigma_\theta = (-\sin\theta, \cos\theta) \begin{pmatrix} \sigma_x & \tau_{xy} \\ \tau_{xy} & \sigma_y \end{pmatrix} \begin{pmatrix} -\sin\theta \\ \cos\theta \end{pmatrix} = \sigma_x \sin^2\theta + \sigma_y \cos^2\theta - 2\tau_{xy} \sin\theta \cos\theta \\ \tau_{r\theta} = (\cos\theta, \sin\theta) \begin{pmatrix} \sigma_x & \tau_{xy} \\ \tau_{xy} & \sigma_y \end{pmatrix} \begin{pmatrix} -\sin\theta \\ \cos\theta \end{pmatrix} = \frac{\sigma_y - \sigma_x}{2} \sin 2\theta + \tau_{xy} \cos 2\theta \end{cases}$$

得到极坐标下的应力边界条件为

$$\begin{cases} \sigma_r(\pm\infty, \theta) = p \cos^2\theta \\ \sigma_\theta(\pm\infty, \theta) = p \sin^2\theta \\ \tau_{r\theta}(\pm\infty, \theta) = -\frac{p}{2} \sin 2\theta \end{cases}$$

应力函数的边值问题可以写为 ~~(不提 σ_θ 的边界条件)~~

$$\begin{cases} \nabla^2 \nabla^2 U = 0 \\ \sigma_r(a, \theta) = 0, \quad \tau_{r\theta}(a, \theta) = 0 \\ \sigma_r(\pm\infty, \theta) = \frac{p}{2} + \frac{p}{2} \cos 2\theta, \quad \tau_{r\theta}(\pm\infty, \theta) = -\frac{p}{2} \sin 2\theta \end{cases}$$

将原问题分解为两个子问题：

$$(1) \begin{cases} \nabla^2 \nabla^2 U^{(1)} = 0 \\ \sigma_r^{(1)}(a, \theta) = 0, \tau_{r\theta}^{(1)}(a, \theta) = 0 \\ \sigma_r^{(1)}(+\infty, \theta) = \frac{P}{2}, \tau_{r\theta}^{(1)}(+\infty, \theta) = 0 \end{cases}$$

$$(2) \begin{cases} \nabla^2 \nabla^2 U^{(2)} = 0 \\ \sigma_r^{(2)}(a, \theta) = 0, \tau_{r\theta}^{(2)}(a, \theta) = 0 \\ \sigma_r^{(2)}(+\infty, \theta) = \frac{P}{2} \cos 2\theta, \tau_{r\theta}^{(2)}(+\infty, \theta) = -\frac{P}{2} \sin 2\theta \end{cases}$$

应力场：第(1)个问题是厚壁圆筒 $b \rightarrow \infty$ 时的情况。

$$\text{应力场} \begin{cases} \sigma_r^{(1)} = \frac{P}{2} \left(1 - \frac{a^2}{r^2}\right) \\ \sigma_\theta^{(1)} = \frac{P}{2} \left(1 + \frac{a^2}{r^2}\right) \\ \tau_{r\theta}^{(1)} = 0 \end{cases}$$

对问题(2)，由应力边值的形式，可设 $U = f(r) \cos 2\theta$

代入双调和方程，展开得

$$f'''' + \frac{2}{r} f'' - \frac{9}{r^2} f'' + \frac{9}{r^3} f' = 0$$

$$\text{通解为 } f(r) = Ar^2 + Br^{-2} + Cr^4 + D$$

$$\text{应力场为} \begin{cases} \sigma_r^{(2)} = \frac{1}{r^2} \frac{\partial^2 U}{\partial \theta^2} + \frac{1}{r} \frac{\partial U}{\partial r} \\ = -(2A + 6Br^{-4} + 4Dr^{-2}) \cos 2\theta \\ \sigma_\theta^{(2)} = \frac{\partial^2 U}{\partial r^2} \\ = (2A + 6Br^{-4} + 12Cr^2) \cos 2\theta \\ \tau_{r\theta}^{(2)} = -\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial U}{\partial \theta} \right) \\ = (2A - 6Br^{-4} + 6Cr^2 - 2Dr^{-2}) \sin 2\theta \end{cases}$$

由应力边条件，解得

$$A = -\frac{P}{4}, \quad B = -\frac{P}{4} a^4$$

$$C = 0, \quad D = \frac{P}{2} a^2$$

$$\text{得应力场} \begin{cases} \sigma_r^{(2)} = \frac{P}{2} \left[1 + 3\left(\frac{a}{r}\right)^4 - 4\left(\frac{a}{r}\right)^2 \right] \cos 2\theta \\ \sigma_\theta^{(2)} = -\frac{P}{2} \left[1 + 3\left(\frac{a}{r}\right)^4 \right] \cos 2\theta \\ \tau_{r\theta}^{(2)} = -\frac{P}{2} \left[1 - 3\left(\frac{a}{r}\right)^4 + 2\left(\frac{a}{r}\right)^2 \right] \sin 2\theta \end{cases}$$

原问题的应力场为

$$\begin{cases} \sigma_r = \frac{p}{2} \left[1 - \left(\frac{a}{r}\right)^2 \right] + \frac{p}{2} \left[1 + 3\left(\frac{a}{r}\right)^4 - 4\left(\frac{a}{r}\right)^2 \right] \cos 2\theta \\ \sigma_\theta = \frac{p}{2} \left[1 + \left(\frac{a}{r}\right)^2 \right] - \frac{p}{2} \left[1 + 3\left(\frac{a}{r}\right)^4 \right] \cos 2\theta \\ \tau_{r\theta} = -\frac{p}{2} \left[1 - 3\left(\frac{a}{r}\right)^4 + 2\left(\frac{a}{r}\right)^2 \right] \sin 2\theta \end{cases} \quad (\sigma_\theta \text{ 的符号由边条件成立})$$

在边界 $r=a$ 上, 环向应力

$$\sigma_\theta = p(1 - 2\cos 2\theta)$$

最大环向应力

$$(\sigma_\theta)_{\max} = \sigma_\theta(a, \pm \frac{\pi}{2}) = 3p$$

应力集中系数

$$k = \frac{(\sigma_\theta)_{\max}}{p} = 3$$

注: 在 X 向拉伸, Y 向压缩时, $\sigma_\theta = p(1 - 2\cos 2\theta) - p(1 + 2\cos 2\theta)$
 $= -4p \cos 2\theta$

$$|(\sigma_\theta)_{\max}| = 4p \quad (\text{在 } \theta = 0, \frac{\pi}{2}, \pi, -\frac{\pi}{2} \text{ 均可达到})$$

应力集中系数 $k = 4$

2° 在 X 向、Y 向均拉伸时, $\sigma_\theta = p(1 - 2\cos 2\theta) + p(1 + 2\cos 2\theta)$
 $= 2p$

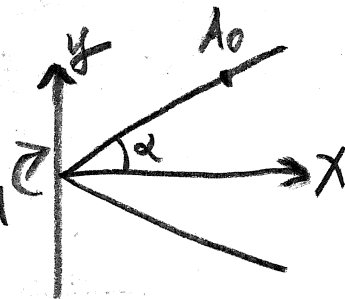
应力集中系数 $k = 2$.

此问题也可用厚壁圆筒解答。

8.6 楔体

① 集中力偶

楔的张角为 2α , 坐标原点为其顶点, X 轴为楔的对称轴。
 集中力偶 M 作用在顶点。



应力函数: 在边界 $\theta = \alpha$ 上任取一点 A_0 , 作为参考点, 令 $\varphi|_{A_0} = \nabla\varphi|_{A_0} = 0$.

则应力函数函数边条件为

$$\begin{cases} \varphi(r, \alpha) = 0, \quad \frac{\partial\varphi}{\partial r}(r, \alpha) = 0, \quad \frac{\partial\varphi}{\partial\theta}(r, \alpha) = 0 \\ \varphi(r, -\alpha) = -M, \quad \frac{\partial\varphi}{\partial r}(r, -\alpha) = 0, \quad \frac{\partial\varphi}{\partial\theta}(r, -\alpha) = 0 \end{cases}$$

∴ 在边界上, 应力函数与 r 无关.

∴ 设 $\varphi = \varphi(\theta)$

双调和函数化为

$$\varphi'''' + 4\varphi'' = 0$$

通解为 $\varphi(\theta) = A + B\theta + C\cos 2\theta + D\sin 2\theta$

代入应力函数边条件

$$\begin{cases} A + B\alpha + C\cos 2\alpha + D\sin 2\alpha = 0 \\ A - B\alpha + C\cos 2\alpha - D\sin 2\alpha = -M \\ B - 2C\sin 2\alpha + 2D\cos 2\alpha = 0 \\ B + 2C\sin 2\alpha + 2D\cos 2\alpha = 0 \end{cases}$$

$$\text{解得 } A = -\frac{M}{2}, \quad B = \frac{-M\cos 2\alpha}{\sin 2\alpha - 2\alpha\cos 2\alpha}$$
$$C = 0, \quad D = \frac{M}{2(\sin 2\alpha - 2\alpha\cos 2\alpha)}$$

应力函数为

$$\varphi(\theta) = -\frac{M}{2} - \frac{M\cos 2\alpha}{\sin 2\alpha - 2\alpha\cos 2\alpha} \theta + \frac{M\sin 2\theta}{2(\sin 2\alpha - 2\alpha\cos 2\alpha)}$$

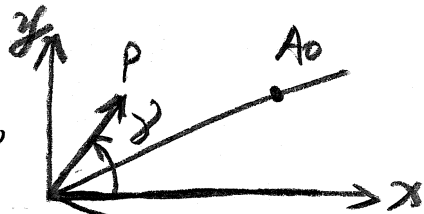
应力场:

$$\begin{aligned} \sigma_r &= \frac{1}{r^2} \frac{\partial^2 \varphi}{\partial \theta^2} + \frac{1}{r} \frac{\partial \varphi}{\partial r} \\ &= \frac{-2M\sin 2\theta}{r^2(\sin 2\alpha - 2\alpha\cos 2\alpha)} \\ \sigma_\theta &= \frac{\partial^2 \varphi}{\partial r^2} = 0 \\ \tau_{r\theta} &= -\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \varphi}{\partial \theta} \right) \\ &= \frac{M(\cos 2\theta - \cos 2\alpha)}{r^2(\sin 2\alpha - 2\alpha\cos 2\alpha)} \end{aligned}$$

注: 用应力函数边值问题的解法可以比较方便地猜出应力函数的形式。

②集中力

同样一个楔，集中力作用在顶点，
角度为 γ 。



应力函数：在边界 $\theta = \alpha$ 上

任取一点 A_0 ，作为参考点，令 $\varphi|_{A_0} = \nabla\varphi|_{A_0} = 0$ 。

则应力函数边界条件为

$$\left\{ \begin{aligned} \varphi(r, \alpha) &= 0, \quad \frac{\partial\varphi}{\partial r}(r, \alpha) = 0, \quad \frac{\partial\varphi}{\partial\theta}(r, \alpha) = 0 \\ \varphi(r, -\alpha) &= -Pr \sin(\alpha + \gamma) \\ \frac{\partial\varphi}{\partial r}(r, -\alpha) &= -P \sin(\alpha + \gamma) \\ \frac{1}{r} \frac{\partial\varphi}{\partial\theta}(r, -\alpha) &= P \cos(\alpha + \gamma) \end{aligned} \right.$$

边界上 [即 $\frac{\partial\varphi}{\partial\theta}(r, -\alpha) = Pr \cos(\alpha + \gamma)$]
由于 $\varphi, \frac{\partial\varphi}{\partial\theta}$ 与 r 成正比, $\frac{\partial\varphi}{\partial r}$ 与 r 无关, 设

$$\varphi = r f(\theta)$$

双调和方程化为

$$f'''' + 2f'' + f = 0$$

通解为 $f(\theta) = A \cos\theta + B \sin\theta + C\theta \cos\theta + D\theta \sin\theta$

代入应力函数边界条件得

$$\left\{ \begin{aligned} A \cos\alpha + B \sin\alpha + C\alpha \cos\alpha + D\alpha \sin\alpha &= 0 \\ -A \sin\alpha + B \cos\alpha + C(\cos\alpha - \alpha \sin\alpha) + D(\sin\alpha + \alpha \cos\alpha) &= 0 \\ A \cos\alpha - B \sin\alpha - C\alpha \cos\alpha + D\alpha \sin\alpha &= -P \sin(\alpha + \gamma) \\ A \sin\alpha + B \cos\alpha + C(\cos\alpha - \alpha \sin\alpha) - D(\sin\alpha + \alpha \cos\alpha) &= P \cos(\alpha + \gamma) \end{aligned} \right.$$

解得 $C = \frac{P \sin\gamma}{2\alpha - \sin 2\alpha}, \quad D = -\frac{P \cos\gamma}{2\alpha + \sin 2\alpha}$

A、B 不影响应力, 所以不用求。

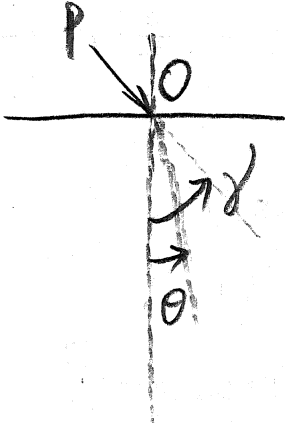
应力函数为 (忽略了含 A、B 的项, 边界条件不再成立, 但不影响应力)

$$\varphi = Pr\theta \left(\frac{\sin\gamma \cos\theta}{2\alpha - \sin 2\alpha} - \frac{\cos\gamma \sin\theta}{2\alpha + \sin 2\alpha} \right)$$

其中 $\varphi = Ar \cos\theta$ 与 $\varphi = Br \sin\theta$
对应 $\varphi = x$ 与 $\varphi = y$,
不产生应力

$$\text{应力场: } \begin{cases} \sigma_r = \frac{1}{r^2} \frac{\partial^2 \varphi}{\partial \theta^2} + \frac{1}{r} \frac{\partial \varphi}{\partial r} \\ = -\frac{2P}{r} \left(\frac{\sin^2 \alpha \sin \theta}{2\alpha - \sin 2\alpha} + \frac{\cos^2 \alpha \cos \theta}{2\alpha + \sin 2\alpha} \right) \\ \sigma_\theta = \frac{\partial^2 \varphi}{\partial r^2} = 0 \\ \tau_{r\theta} = -\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \varphi}{\partial \theta} \right) = 0 \end{cases}$$

注: 1° Boussinesq 问题



集中力作用在半平面边界上的问题称为 Boussinesq 问题。

α 取 π/2 时的楔体受集中力作用的问题与 Boussinesq 问题相同。

$$\text{应力场: } \begin{cases} \sigma_r = -\frac{2P}{\pi r} (\sin^2 \alpha \sin \theta + \cos^2 \alpha \cos \theta) \\ \sigma_\theta = \tau_{r\theta} = 0 \end{cases}$$

垂直于半平面边界时,

$$\begin{cases} \sigma_r = -\frac{2P \cos \theta}{\pi r} \\ \sigma_\theta = \tau_{r\theta} = 0 \end{cases}$$

平行于半平面边界时,

$$\begin{cases} \sigma_r = -\frac{2P \sin \theta}{\pi r} \\ \sigma_\theta = \tau_{r\theta} = 0 \end{cases}$$