

大纲

Saint-Venant 问题

$$\iint_{\Omega} \frac{\partial \Psi}{\partial x_i} dx dy = \oint_{\partial \Omega} \Psi \cos \langle \vec{n}, \vec{x}_i \rangle ds$$

(高斯公式的环路积分为要标明外法向)

翘曲函数问题

$$\nabla^2 \varphi = 0$$

$$\frac{\partial \varphi}{\partial n} = y \cos \langle \vec{n}, \hat{x} \rangle - x \cos \langle \vec{n}, \hat{y} \rangle = (y, -x) \cdot \vec{n}$$

$$D = \iint_{\Omega} (x^2 + y^2 + x \frac{\partial \varphi}{\partial y} - y \frac{\partial \varphi}{\partial x}) dx dy = \iint_{\Omega} [x^2 + y^2 + (y, -x) \cdot \nabla \varphi] dx dy$$

位势场

$$\begin{cases} u_r = 0 \\ u_\theta = \alpha r z \\ u_z = \alpha \varphi \end{cases}$$

扭转刚度恒正。

(证明: $C_i > 0$)
 Ψ 的位势单值性条件)

最大剪应力在边界上达到。



(证明: $\nabla^2(\tau^2) > 0$)

~~若域内某点处的剪应力不是~~

$$\oint \tau ds = 2\mu\alpha A$$

等周线

(证明: 与位势单值性条件一致)



区域	Ψ
	$k(1 - \frac{x^2}{a^2} - \frac{y^2}{b^2})$
	... $-\frac{1}{2} \cdot \frac{r+\delta}{r} \cdot (r-\delta)(r-2a\cos\theta)$

$$\text{圆的扭转刚度 } D = \frac{\pi a^4}{2}$$

$$\tau_{max} = \mu\alpha a$$

带圆槽圆杆

$$\tau_{max} \approx 2\mu\alpha a$$

区域	Ψ
	$(\frac{\delta}{z})^2 - \eta^2$
	$-\frac{2A}{l}(\eta - \frac{\delta}{z})$

$$J_{\text{环}} : D = \frac{1}{3} l \delta^3$$

$$\frac{J_{\text{环}}}{D_{\text{圆}}} \propto (\frac{\delta}{a})^2$$

上下界定理

证明: 上界定理:

$$I(\varphi) = D + I_1(\varphi)$$

$$I_1(\varphi) = 0$$

运用 $\nabla^2 \varphi = 0$

$$\frac{\partial \varphi}{\partial n} = (y, -x) \cdot \vec{n}$$

$$I(\varphi) = I_1(\varphi) + 0 + (\geq 0)$$

下界定理:

$$J(\Psi) = D - J_1(\Psi)$$

$$J_1(\Psi) = 0$$

证明 $\nabla^2 \Psi = -2$

$$\begin{cases} \Psi|_{L_i} = C_i \\ \oint_{L_i} \frac{\partial \Psi}{\partial n} ds = 2A_i \end{cases}$$

$$J(\Psi) = J_1(\Psi) + 0 - (\geq 0)$$

$$I_1(\varphi) = \iint_{\Omega} \nabla \cdot [\nabla \varphi - (y, -x)] dx dy$$

$$J_1(\Psi) = \iint_{\Omega} \nabla \cdot [\nabla \Psi + (y, -x)] dx dy = 2 \sum C_i A_i$$

$$\begin{cases} \nabla^2 \Psi = -2 \\ \Psi|_{L_0} = 0, \Psi|_{L_i} = C_i \end{cases}$$

($i=1, 2, \dots, m$)

$$\oint_{L_i} \frac{d\Psi}{dn} ds = 2A_i$$

($i=1, 2, \dots, m$)

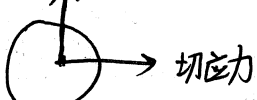
(在物单值性条件用非定常数 C_i)

$$D = 2 \left(\iint_{\Omega} \Psi dx dy + \sum_{i=1}^m C_i A_i \right)$$

$$\alpha = \frac{M_z}{\mu D}$$

$$\tau_{zx} = \mu \alpha \frac{\partial \Psi}{\partial y}, \tau_{zy} = -\mu \alpha \frac{\partial \Psi}{\partial x}$$

Ψ 偏数 $\times \mu \alpha$



$$\tau_r = \mu \alpha \frac{\partial \Psi}{\partial r \partial \theta}, \tau_\theta = -\mu \alpha \frac{\partial \Psi}{\partial r}$$

Ψ :

$$\Psi = \underline{\Psi} + \frac{1}{2}(x^2 + y^2)$$

$$\begin{cases} \frac{\partial \Psi}{\partial x} = \frac{\partial \underline{\Psi}}{\partial x} + x \\ \frac{\partial \Psi}{\partial y} = \frac{\partial \underline{\Psi}}{\partial y} + y \end{cases}$$

$$\varphi = \begin{cases} \frac{\partial \varphi}{\partial x} = \frac{\partial \underline{\varphi}}{\partial x} \\ \frac{\partial \varphi}{\partial y} = -\frac{\partial \underline{\varphi}}{\partial y} \end{cases} \quad (\text{Ca-R 方程})$$

$$\varphi = -\text{Im} \{ \psi(z, 0) \}$$

平面-直角

本构关系

$$\begin{cases} \epsilon_x = \frac{1}{E} (\sigma_x - \nu \sigma_y) \\ \epsilon_y = \frac{1}{E} (\sigma_y - \nu \sigma_x) \\ \epsilon_{xy} = \frac{1+\nu}{E} \tau_{xy} \end{cases}$$

注: 对平面应力问题, 上式直接使用
对平面应变问题, 作代换

$$\begin{cases} E' = \frac{E}{1-\nu^2} \\ \nu' = \frac{\nu}{1-\nu} \end{cases}$$

$$\begin{cases} \sigma_x = \frac{E}{1-\nu^2} (\epsilon_x + \nu \epsilon_y) \\ \sigma_y = \frac{E}{1-\nu^2} (\epsilon_y + \nu \epsilon_x) \\ \tau_{xy} = \frac{E}{1+\nu} \epsilon_{xy} \end{cases}$$

注: 同上.

平衡方程

$$\begin{cases} \frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + f_x = 0 \\ \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + f_y = 0 \end{cases}$$

应变协调方程

$$\epsilon_{xx,yy} + \epsilon_{yy,xx} = 2 \epsilon_{xy,xy}$$

应力协调方程 ($\vec{f} = \text{常量}$)

$$\nabla^2 (\sigma_x + \sigma_y) = 0$$

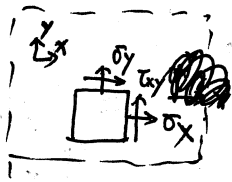
平面应力问题与平面应变问题基本方程组的差异:

平面应力	平面应变
协调方程	
$\epsilon_{zz,xx} = \epsilon_{zz,yy} = 0$	
$\epsilon_{zz,xy} = 0$	
	几何约束: $\epsilon_{zz} = \epsilon_x$ $\epsilon_{zz} = \epsilon_y$

平面应力	平面应变
	本构关系 $\sigma_z = \nu(\sigma_x + \sigma_y)$

应力与应力函数间关系

$$\begin{cases} \sigma_x = \frac{\partial^2 U}{\partial y^2} \\ \sigma_y = \frac{\partial^2 U}{\partial x^2} \\ \tau_{xy} = -\frac{\partial^2 U}{\partial x \partial y} \end{cases}$$



平面问题的提法

$$\begin{cases} \nabla^2 U = 0 & (G) \\ \text{应力边界条件} & (\partial G) \end{cases}$$

或

$$\begin{cases} \nabla^2 \nabla^2 U = 0 & (G) \\ \text{应力函数边界条件} & (\partial G) \end{cases}$$

应力函数 U 的性质:

- 1° 线性函数不影响应力场;
可以任取一个标准参考点 A_0
- 2° 应力函数梯度的边界值与边界段 A_0A_1 上的载荷主向量具有关系

$$\nabla \varphi|_{A_0A_1} \rightarrow \vec{R}|_{A_0A_1}$$
- 3° 应力函数的边界值与边界段 A_0A_1 上的主矩 (以 A_0 为参考点) 相等。

$$\varphi|_{A_1} = M_1$$

- 注: ① 应用条件: Oxy 为平面右手系
2° 从 A_0 点逆时针转到 A_1 点。
② 如果用右手顺时针转, 则上述结论
2°, 3° 反号。

若应力边界条件为

$$\vec{f} = (f_x, f_y) = \text{常量}$$

$$\vec{f} = (t_x, t_y)$$

则问题分解为

$$(1) \begin{cases} \vec{f}^{(1)} = (f_x, f_y) \\ \vec{f}^{(2)} = (\tilde{t}_x, \tilde{t}_y) \end{cases}$$

待解
$$\begin{cases} \sigma_x = -f_x x \\ \sigma_y = -f_y y \\ \tau_{xy} = 0 \end{cases} \begin{cases} \sigma_x = 0 \\ \sigma_y = 0 \\ \tau_{xy} = -f_x y - f_y x \end{cases}$$

(满足平衡方程和应力协调方程)
$$\nabla^2 (\sigma_x + \sigma_y) = 0$$

应力边界条件由特解解决。

$$(2) \begin{cases} \vec{f}^{(2)} = 0 \\ \vec{f}^{(2)} = (t_x - \tilde{t}_x, t_y - \tilde{t}_y) \end{cases}$$

可用一般平面问题的解法做

平面-直角问题的备选解决方案:

- 1° 应力函数边值问题
- 2° 应力函数形式 \rightarrow 应力场 \rightarrow 定系数

问题	应力函数
M, P, q	$C_1 (M + Px + \frac{1}{2} q x^2) + f(y)$ $+ C_2 q g(y)$ 其中: $f(y) = \int \int \dots$ 二次 $g(y) = \int \int \dots$ 五次 $g(y) = y(y - \frac{1}{2})^2$
f_1, f_2, f_0	$\frac{x^2}{2} f_2(y) + x f_1(y) + f_0(y)$ ($\sigma_y = f_2(y)$)
Δ	$P_3(x, y)$ (应力为线性函数)

平面 - 极坐标

几何方程

$$\begin{cases} \epsilon_r = \frac{\partial u_r}{\partial r} \\ \epsilon_\theta = \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{u_r}{r} \\ \epsilon_{r\theta} = \frac{1}{2} \left(\frac{\partial u_\theta}{\partial r} + \frac{1}{r} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta}{r} \right) \end{cases}$$

平衡方程

$$\begin{cases} \frac{\partial \sigma_r}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\theta}}{\partial \theta} + \frac{\sigma_r - \sigma_\theta}{r} + f_r = 0 \\ \frac{\partial \tau_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_\theta}{\partial \theta} + \frac{2\tau_{r\theta}}{r} + f_\theta = 0 \end{cases}$$

本构关系

$$\begin{cases} \epsilon_r = \frac{1}{E} (\sigma_r - \nu \sigma_\theta) \\ \epsilon_\theta = \frac{1}{E} (\sigma_\theta - \nu \sigma_r) \\ \epsilon_{r\theta} = \frac{1+\nu}{E} \tau_{r\theta} \\ \sigma_r = \frac{E}{1-\nu^2} (\epsilon_r + \nu \epsilon_\theta) \\ \sigma_\theta = \frac{E}{1-\nu^2} (\epsilon_\theta + \nu \epsilon_r) \\ \tau_{r\theta} = \frac{E}{1+\nu} \epsilon_{r\theta} \end{cases}$$

注: 对平面应变问题, 同样作代换.

应力协调方程

$$\nabla^2 (\sigma_r + \sigma_\theta) = 0$$

应力与应力函数间关系:

$$\begin{cases} \sigma_r = \frac{1}{r^2} \frac{\partial^2 U}{\partial \theta^2} + \frac{1}{r} \frac{\partial u}{\partial r} \\ \sigma_\theta = \frac{\partial^2 U}{\partial r^2} \\ \tau_{r\theta} = -\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial U}{\partial \theta} \right) \end{cases}$$

平面问题的提法

$$\begin{cases} \nabla^2 U = 0 & (G) & \text{(主要)} \\ \text{应力边界条件} & (2G) & \\ \nabla^2 U = 0 & (G) & \\ \text{应力函数边界条件} & (2G) & \text{(偶解)} \end{cases}$$

① 轴对称应力问题 (厚壁圆筒; 曲梁纯弯曲)

$$U = U(r) \quad \langle 0, 0 \rangle$$

$$\begin{aligned} \text{通解 } U &= A + B \ln r + Cr^2 + Dr^2 \ln r \\ \text{应力场 } \begin{cases} \sigma_r = \frac{B}{r^2} + D(1+2\ln r) + 2C \\ \sigma_\theta = -\frac{B}{r^2} + D(3+2\ln r) + 2C \\ \tau_{r\theta} = 0 \end{cases} \end{aligned}$$

几何、变力/几何约束轴对称时的

$$\begin{aligned} \text{应力场 } \begin{cases} \sigma_r = \frac{B}{r^2} + 2C \\ \sigma_\theta = -\frac{B}{r^2} + 2C \\ \tau_{r\theta} = 0 \end{cases} \\ \text{位移场 (不考虑刚体位移)} \\ \begin{cases} u_r = \frac{1}{E} \left[-(1+\nu) \frac{B}{r} + 2(1-\nu) Cr \right] \\ u_\theta = 0 \end{cases} \end{aligned}$$

有圆孔的无限大板双向拉伸

$$\begin{aligned} \text{应力场 } \begin{cases} \sigma_r = (1 - \frac{a^2}{r^2}) p_0 \\ \sigma_\theta = (1 + \frac{a^2}{r^2}) p_0 \\ \tau_{r\theta} = 0 \end{cases} \\ k=2 \end{aligned}$$

② 曲梁受切向力

$$U = f(r) \sin \theta \quad \langle 1, -1 \rangle$$

$$\text{通解 } U = (Ar + Br^{-1} + Cr^3 + Dr \ln r) \sin \theta$$

③ 有圆孔的无限大板单向拉伸

$$U = f(r) \cos 2\theta \quad \langle 2, -2 \rangle$$

$$\begin{aligned} \text{通解 } U &= (Ar^2 + Br^{-2} + Cr^4 + D) \cos 2\theta \\ \text{内边界 } r=a \text{ 上的环向应力} \\ \sigma_\theta &= p(1-2\cos 2\theta) \\ k &= 3 \end{aligned}$$

④ 楔体受集中力偶

$$U = U(\theta)$$

$$\text{通解 } U(\theta) = A + B\theta + C \cos 2\theta + D \sin 2\theta$$

⑤ 楔体受集中力

$$U = r f(\theta)$$

$$\text{通解 } U = r(A \cos \theta + B \sin \theta + C \cos 3\theta + D \sin 3\theta)$$

Boussinesq 问题:

$$\begin{aligned} \text{力垂直边界} \\ \begin{cases} \sigma_r = -\frac{2P \cos \theta}{\pi r} \\ \sigma_\theta = \tau_{r\theta} = 0 \end{cases} \\ \text{力平行边界} \\ \begin{cases} \sigma_r = -\frac{2P \sin \theta}{\pi r} \\ \sigma_\theta = \tau_{r\theta} = 0 \end{cases} \end{aligned}$$

⑥ 楔体受均布力

$$\begin{aligned} U &= r^2 f(\theta) \\ \text{通解 } U &= r^2(A + B\theta + C \cos 2\theta + D \sin 2\theta) \end{aligned}$$

⑦ 楔体受线性分布力

$$\begin{aligned} U &= r^3 f(\theta) \\ \text{(或用三角形水坝的解)} \\ \text{通解 } U &= r^3(A \cos 3\theta + B \sin 3\theta + C \cos 3\theta + D \sin 3\theta) \end{aligned}$$

积分表

$$\int \frac{dx}{\cos^2 x} = \tan x + C$$

$$\int \frac{dx}{\sin^2 x} = -\cot x + C$$

$$\int \frac{dx}{1+x^2} = \arctan x + C$$

$$\int \frac{dx}{\sqrt{1-x^2}} = \arcsin x + C$$

$$\int \frac{dx}{\sqrt{x^2 \pm a^2}} = \ln|x + \sqrt{x^2 \pm a^2}| + C$$

$$\int \ln x dx = x(\ln x - 1) + C$$